Irada G. Malikova et al./ Elixir Appl. Chem. 99 (2016) 43300-43304

Available online at www.elixirpublishers.com (Elixir International Journal)



Applied Chemistry





Mechanism and Kinetic Model of Heterogeneous Catalystic Process of Demercaptanization of Oil

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| ARTICLE INFO |
|-----------------------------|
| Article history: |
| Received: 5 September 2016; |
| Received in revised form: |
| 29 February 2016; |
| Accepted: 2 March 2016; |

ABSTRACT

New heterogeneous and catalytic systems were obtained and their activities were further studied to ensure process of a demercaptanization (mercaptan removal) of oil and oil products. Kinetic regularities of a process were researched. The kinetic model and the mechanism of a demercaptanization of an ethyl mercaptan as a model reaction with participation of organic ligand catalyst deposited on clinoptilolite So-Fe, Mn-Fe is suggested by this study.

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Clinoptilolite, Catalyst,

Systems,

Keywords

Demercaptanization, Heterogeneous Catalystic

Kinetic Model.

Introduction

Mercaptan compounds having the composition of oil and oil products have negative impact on the quality of petroleum products and are the cause of the equipment corrosion used during their production, transportation and processing, which eventually leads to their failure and create environmental problems. Despite the fact that there have been many ways developed to purge oil and oil products from other sulfur compounds, the mercaptan sweetening has been studied marginally. Mercaptan sweetening is currently supplied mainly by classical chemical methods, i.e. using the alkaline and acidic reagents and is conducted by neutralization method. However, this method cannot clean mercaptans over 50-60%, furthermore, these processes require a great number of reagents, solutions and others. Moreover, there are a number of technological problems. In recent years, process of demercaptanization involving catalysts has drawn attention. Herein, aluminum-silicate catalysts are being generally used and the process is conducted at very high temperatures of 800-1000°C involving hydrogen. The most commonly used catalyst is the catalyst system in the form of Co, Mo, Ni-Mo, MoS₂ deposited on aluminum oxide. These catalytic systems showing high activity at high temperatures require large energy costs, their regeneration after catalyst deactivation passes with difficulty. From this standpoint, we set the task of creation of catalytic systems on the basis of local raw materials for processes of a demercaptanization.

2. Methods and Apparatus

For demercaptanization of oil products were obtained catalyst systems based on Mo, Co, V, Ni, P oxides and organic ligands of Co, Mn, Fe deposited Al₂O₃, SiO₂, mordenite, and their activities were revealed in demercaptanization process [12,13]. The obtained results are presented in Table 1. It

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should be noted that mercaptan compounds of C_1-C_4 present in the composition of oil products have generally been subject to demercaptanization. Thiophene units of oil were subjected to demercaptanization. Kinetic regularities of the process were studied within a wide range of alterations to key parameters. Initially, the model system was prepared consisting of ethyl mercaptan dissolved in light oil. Some samples of 0.2–0.6 g/l from quantity of an ethyl mercaptan close to real fraction of benzine were prepared. Note that both originally taken substances and obtained compounds were controlled by chromatographic, IR analysis and other methods of analysis. Thus it is possible to identify process indicators, by definition of amount of the obtained free sulfur and saturated hydrocarbons as the main indicators.

| Table | 1. Study | of the | activity | of th | e catalyst | system | in |
|------------|------------|--------|----------|--------|-------------|--------|----|
| the proces | s of the d | emerca | aptaniza | tion a | of oil prod | ucts. | |

| the process of the demercaptanization of on products. | | | | | | |
|---|---------------|---|---------------|--|--|--|
| Catalyst systems | Purification | Catalyst systems | Purification | | | |
| | efficiency of | | efficiency of | | | |
| | benzine | | benzine | | | |
| MoO ₃ /Al ₂ O ₃ | 68 | Fe-Mo/Al ₂ O ₃ | 75 | | | |
| V_2O_5/Al_2O_3 | 60 | Ni-MoO ₃ /Al ₂ O ₃ | 70 | | | |
| MoO ₃ /SiO ₂ | 64 | MoO ₃ /klinoptilolite | 75 | | | |
| V ₂ O ₅ /SiO ₂ | 60 | Co ₂ O ₃ /klinoptilolite | 72 | | | |
| V-P-O/Al ₂ O ₃ | 62 | Co-Fe/klinoptilolite | 92 | | | |
| V-P-O/SiO ₂ | 60 | Mn-Fe/klinoptilolite | 86 | | | |
| V-Mo-O/Al ₂ O ₃ | 72 | MoO ₃ / mordenite | 60 | | | |
| V-Mo-O/SiO ₂ | 70 | Co ₂ O ₃ / mordenite | 60 | | | |
| Co-Mo/Al ₂ O ₃ | 74 | Co-Fe/ mordenite | 74 | | | |
| Mn-Fe/Al ₂ O ₃ | 76 | Mn-Fe/ mordenite | 78 | | | |

3. Experimental

The influence of the temperature on conversion level of an ethyl mercaptan, i.e. influence on the degree of purification of benzene has been studied in order to study the kinetic regularities of the process of a demercaptanization. Taking into account the change of ethyl and propyl mercaptans in the low-boiling fraction of 303–3530K of benzine in the range 0.2–0.6 g/l influence of temperature on process of demercaptanization was studied.

4. Results and Discussion

The results (table 2–4, fig. 1) show that in the presence of MoO_3/Al_2O_3 , V_2O_5 –Mo– O_3/Al_2O_3 , $Co_2O_3/$ clinoptilolite, $MnO_2/$ clinoptilolite, etc. at the temperature of 313K ethyl mercaptan conversion varies in the range 70–80% and the temperature increase from 323K to 333K leads to some increase of ethyl mercaptan conversions up to 80–85%.

| Table 2. Demercaptanization of ethyl mercaptan | with |
|--|-------------------|
| participation of various catalysts, $T = 313K$, $V =$ | 10h ⁻¹ |

| Catalytic system | conversion, % | Amount of S, obtained in the | | Amount of obtained alkane | |
|--|------------------|---------------------------------|-------------|------------------------------|---------|
| - | | demerca | ptanization | | |
| | | q | mol | q | mol |
| MoO ₃ /Al ₂ O ₃ | 72 | 0.071 | 0.0022 | 0.063 | 0.0011 |
| MoO ₃ /SiO ₂ | 70 | 0.070 | 0.021 | 0.058 | 0.0110 |
| V ₂ O ₅ - | 75 | 0.077 | 0.024 | 0.069 | 0.0012 |
| MoO ₃ /Al ₂ O ₃ | | | | | |
| Co-MoO ₃ | 76 | 0.078 | 0.025 | 0.070 | 0.00121 |
| /Al ₂ O ₃ | | | | | |
| Fe- | 73 | 0.074 | 0.0023 | 0.062 | 0.0012 |
| MoO ₃ /Al ₂ O ₃ | | | | | |
| MoO ₃ / | 77 | 0.083 | 0.0026 | 0.072 | 0.0013 |
| clinoptilolite | | | | | |
| Co ₂ O ₃ / | 75 | 0.077 | 0.0024 | 0.077 | 0.00123 |
| clinoptilolite | | | | | |
| MnO ₂ / | 78 | 0.080 | 0.025 | 0.074 | 0.00125 |
| clinoptilolite | | | | | |
| Co:Fe/ | 96 | 0.098 | 0.0030 | 0.086 | 0.00154 |
| clinoptilolite | | | | | |
| Mn–Fe/ | 95 | 0.090 | 0.028 | 0.073 | 0.00146 |
| clinoptilolite | | | | | |

Table 3. Demercaptanization of ethyl mercaptan with participation of various catalysts. T = 313K, $V = 10h^{-1}$

| participa | participation of various catalysis, 1 – 515K, V – 10h | | | | | | | |
|--|---|-----------------|------------|-----------|-------|--|--|--|
| Catalytic | conversion, | Amou | nt of S, | Amount of | | | | |
| system | % | obtained in the | | obtained | | | | |
| | | demercap | tanization | alka | nes | | | |
| | | q | mol | q | mol | | | |
| MoO ₃ /Al ₂ O ₃ | 76 | 0.0025 | 0.0078 | 0.0012 | 0.070 | | | |
| MoO ₃ /SiO ₂ | 74 | 0.0023 | 0.074 | 0.0011 | 0.062 | | | |
| V_2O_5- | 80 | 0.0026 | 0.082 | 0.0013 | 0.075 | | | |
| MoO ₃ /Al ₂ O ₃ | | | | | | | | |
| Co–MoO ₃ | 80 | 0.0026 | 0.082 | 0.0013 | 0.075 | | | |
| /Al ₂ O ₃ | | | | | | | | |
| Fe- | 73 | 0.025 | 0.0078 | 0.0012 | 0.070 | | | |
| MoO ₃ /Al ₂ O ₃ | | | | | | | | |
| MoO ₃ / | 80 | 0.026 | 0.0082 | 0.0013 | 0.075 | | | |
| clinoptilolite | | | | | | | | |
| Co ₂ O ₃ / | 78 | 0.026 | 0.0081 | 0.0030 | 0.072 | | | |
| clinoptilolite | | | | | | | | |
| MnO ₂ / | 82 | 0.027 | 0.0082 | 0.0014 | 0.073 | | | |
| clinoptilolite | | | | | | | | |
| Co:Fe/ | 98 | 0.016 | 0.0097 | 0.0152 | 0.092 | | | |
| clinoptilolite | | | | | | | | |
| Mn-Fe/ | 97 | 0.014 | 0.0096 | 0.0150 | 0.090 | | | |
| clinoptilolite | | | | | | | | |

Only a catalytic system obtained by depositing organic ligand of Mn–Fe and Co–Fe on clinoptilolite at low temperatures allow to reach conversion of ethyl mercaptan about 94–95% and at relatively high temperatures 333°K conversion of 99%. It was studied the influence of the contact time on the activity of those catalytic systems that have a relatively high activity among obtained. As seen from the results of studies (Figure 2), the catalyst system in a contact time of 8–10 minutes shows high activity and provides conversion of ethyl mercaptan to the level of 98–99%. Relatively high demercaptanization of prepared model

systems in the table 1 is explained due to the presence in the benzine composition of other impurities.

| Table 4. Demercaptanization of ethyl mercaptan wit | h |
|--|---|
|--|---|

| participation of various catalysts, $T = 353K$, $V = 10h^{-1}$ | | | | | | | |
|---|-------------|-----------|-----------|-----------|----------|--|--|
| Catalytic | conversion, | Amoun | t of S, | Amount of | | | |
| system | % | obtained | l in the | obtai | obtained | | |
| | | demercapt | anization | alka | nes | | |
| | | q | mol | q | mol | | |
| MoO ₃ /Al ₂ O ₃ | 80 | 0.0025 | 0.082 | 0.0013 | 0.075 | | |
| MoO ₃ /SiO ₂ | 76 | 0.0023 | 0.078 | 0.0012 | 0.070 | | |
| V_2O_5- | 84 | 0.0026 | 0.097 | 0.0013 | 0.078 | | |
| MoO ₃ /Al ₂ O ₃ | | | | | | | |
| Co-MoO ₃ | 85 | 0.0027 | 0.098 | 0.0013 | 0.079 | | |
| /Al ₂ O ₃ | | | | | | | |
| Fe- | 78 | 0.0025 | 0.090 | 0.0012 | 0.072 | | |
| MoO ₃ /Al ₂ O ₃ | | | | | | | |
| MoO ₃ / | 85 | 0.0027 | 0.098 | 0.0013 | 0.079 | | |
| clinoptilolite | | | | | | | |
| Co ₂ O ₃ / | 80 | 0.0025 | 0.082 | 0.0013 | 0.075 | | |
| clinoptilolite | | | | | | | |
| MnO ₂ / | 90 | 0.0026 | 0.099 | 0.0013 | 0.078 | | |
| clinoptilolite | | | | | | | |
| Co:Fe/ | 99 | 0.0031 | 0.102 | 0.0016 | 0.093 | | |
| clinoptilolite | | | | | | | |
| Mn–Fe/ | 99 | 0.102 | 0.0031 | 0.0016 | 0.093 | | |
| clinoptilolite | | | | | | | |



Fig 1. Effect of temperature on the activity of the catalyst system in the process of demercaptanization of ethyl mercaptan. 1–MoO₃/Al₂O₃, 2 – MoO₃/SiO₂, 3 – V₂O₅–MoO₃/Al₂O₃, 4–Co-MoO₃/Al₂O₃, 5–Fe–MoO₃/Al₂O₃, 6–MoO₃/klinop, 7–Co₂O₃/klinop., 8–MnO₂/clinoptilolite, 9 – Co: Fe clinoptilolite, 10 – Mn–Fe/clinoptilolite.



Fig 2. Influence of contact time on the activity of a catalyst in demercaptanization ethyl mercaptan. 1–MoO₃/Al₂O₃, 2–Co–MoO₃/Al₂O₃, 3–MnO₂/clinoptilolite, 4–Mn–Fe/ clinoptilolite, 5–Fe–Co/clinoptilolite.

1.
$$C_{2}H_{3}SH + Z \leftarrow \frac{k_{1}}{k_{1}} (C_{2}H_{3}SH)Z$$

AZ
2. $2[C_{2}H_{3}SH_{1}Z + O_{2} \leftarrow \frac{k_{2}}{k_{2}} + ZC_{2}H_{3} + C_{2}H_{5} + S + [H_{2}O]Z$
AZ
R
3. $ZC_{3}H_{3}C_{3}H_{3} \leftarrow \frac{k_{2}}{k_{3}} + C_{2}C_{2}H_{10} + Z$
ZR
4. $[C_{2}H_{3}SH]Z + O_{2} \leftarrow \frac{k_{1}}{k_{2}} + 2CO_{2} + S + 3[H_{3}O]Z$
5. $[H_{2}O]Z \leftrightarrow H_{2}O + Z$
6. $2[C_{2}H_{3}SH]Z + H_{2}O - \frac{k_{2}}{k_{0}} + C(C_{2}H_{6}) + S + [C_{2}H_{5}OH]Z$
AZ
7. $2[C_{2}H_{3}SH]Z + O_{2} - \frac{k_{2}}{k_{2}}]CH_{2} = CH_{2}]Z + [C_{2}H_{5}OH]Z$
AZ
7. $2[C_{2}H_{5}SH]Z + O_{2} - \frac{k_{2}}{k_{2}}]CC_{2}H_{5}OC_{2}H_{5}] + H_{2}O$
8. $[CH_{2} = CH_{2}]Z \leftarrow \frac{k_{2}}{k_{8}} + D + Z$
9. $2[C_{2}H_{5}OH]Z + H_{2}O - \frac{k_{2}}{k_{0}} + Z[C_{2}H_{5}OC_{2}H_{5}] + H_{2}O$
10. $Z[C_{2}H_{6}] \leftarrow \frac{k_{10}}{k_{10}}F + Z$
11. $Z(C_{2}H_{5}OH) + C_{2}H_{5}OC_{2}H_{5} + Z$
12. $Z(C_{3}H_{5}OH) \leftrightarrow C_{2}H_{5}OC_{2}H_{5} + Z$
12. $Z(C_{3}H_{5}OH) \leftrightarrow C_{2}H_{5}OC_{2}H_{5} + Z$
13. $Z(C_{3}H_{5}OH) \leftrightarrow C_{2}H_{5}OC_{2}H_{5} + Z$
14. $Z(C_{3}H_{5}OH) \leftrightarrow C_{2}H_{5}OC_{2}H_{5} + Z$
15. $Z(C_{3}H_{5}OH) \leftrightarrow C_{2}H_{5}OC_{2}H_{5} + Z$
16. $W_{1} = K_{1}P_{A} \cdot C_{Z} - K_{3}C_{AZ}$
 $W_{3} = K_{5}C_{Z}H_{5}O_{2}$
 $W_{4} = K_{4}C_{AR}P_{O_{2}}$
 $W_{5} = K_{5}C_{Z}H_{5}O + K_{5}P_{H_{5}O}C_{Z}$
 $W_{6} = K_{6}C_{[AZ]} \cdot P_{H_{2}O}$
 $W_{7} = K_{7}C_{AZ}^{2} \cdot P_{O_{2}}$
 $W_{8} = K_{6}C_{[ZZ} - K_{4}B_{P}C_{Z}$
 $W_{9} = K_{9}C_{EZ} - K_{4}B_{P}C_{Z}$
 $W_{1} = K_{1}C_{ZN} - K_{4}B_{P}C_{Z}$
 $W_{2} = K_{2}C$

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$$\begin{split} C_{AZ} &= \frac{\pm [K_{-1} + K_4] \pm \sqrt{(K_2 + K_6 P_{H,0} + K_7 P_{0_2})^2 + 4(K_2 + K_6 P_{H,0} + K_7}{2[K_2 + K_6 P_{H,0} + K_7 P_{0_2}]} \\ \frac{d_{RZ}}{d\tau} &= K_2 C_{AZ}^2 P_{0_2} + K_{-3} C_Z P_R - K_3 C_{RZ} \\ C_{RZ} &= \frac{K_2 C_{AZ}^2 P_{0_2} + K_{-3} C_Z P_R}{k_3} \\ \frac{dC_{AZ}}{d\tau} &= K_7 C_{AZ}^2 P_{0_2} + K_{-8} C_D C_Z - K_8 C_{DZ} \\ C_{DZ} &= \frac{K_7 C_{AZ}^2 P_{0_2} + K_{-8} P_D C_Z}{k_8} \\ \frac{d \frac{C_{EZ}}{d\tau} = K_7 C_{EZ} - K_9 C_{EZ}^2 + K_9 C_{NZ} P_{H,0} - K_9 C_{EZ}^2 - K_7 C_{EZ} + K_{-9} C_{NZ} P_{H,0} \\ C_{EZ}^2 &= \frac{K_7 C_{EZ} + K_9 C_{NZ} P_{H,0}}{k_9} \\ \frac{d \frac{C_{FZ}}{d\tau} = K_6 C_{AZ}^2 P_{H,0} + K_{-10} P_F C_Z - K_{10} C_{FZ} \\ C_{FZ} &= \frac{K_6 C_{AZ}^2 P_{H,0} + K_{-10} P_F C_Z}{k_{10}} \\ \frac{d \frac{C_{NZ}}{d\tau} = K_9 C_{AZ}^2 - K_{-9} C_{NZ} P_{H,0} + K_{-11} P_N C_Z - K_{11} C_{NZ} \\ C_{NZ} &= \frac{K_9 C_{AZ}^2 - K_{-9} C_{NZ} P_{H,0} + K_{-11} P_N C_Z - K_{11} C_{NZ} \\ \frac{d \frac{C_{ZZ}}{d\tau} = K_{-1} C_{AZ} - K_1 C_Z P_A + K_{-3} C_{ZR} - K_3 P_R C_Z + K_8 C_{DZ} - K_{-12} P_E C_Z \\ C_{RZ} &= \frac{K_{-1} C_{AZ} - K_{10} C_Z P_F + K_{11} C_{ZN} - K_{-11} C_Z P_N + K_{12} C_{EZ} - K_{-12} P_E C_Z \\ C_{Z} &= \frac{K_{-1} C_{AZ} - K_{-3} C_{ZR} + K_8 C_{DZ} + K_{10} C_{ZF} + K_{11} C_{ZN} + K_{12} C_{EZ} - K_{-12} P_E C_Z \\ C_{Z} &= \frac{K_{-1} C_{AZ} + K_{-3} C_{ZR} + K_8 C_{DZ} + K_{10} C_{ZF} + K_{11} C_{ZN} + K_{12} C_{EZ} - K_{-12} P_E C_Z \\ C_{Z} &= \frac{K_{-1} C_{AZ} + K_{-3} C_{ZR} + K_8 C_{DZ} + K_{10} C_{ZF} + K_{11} C_{ZN} + K_{12} C_{EZ} - K_{-12} P_E C_Z \\ C_{Z} &= \frac{K_{-1} C_{AZ} + K_{-3} C_{ZR} + K_8 C_{DZ} + K_{-10} P_F + K_{-11} P_N + K_{12} P_E \\ \frac{dC_{1H,0H}}{d\tau} &= K_2 C_{AZ}^2 P_{0_2} + K_4 C_{AZ} P_{0_2} + K_{-5} P_{H_2} C_Z - K_5 C_{(H_20)1} \\ C_{Z} + C_{AZ} + C_{RZ} + C_{(H_20)1} + C_{FZ} + C_{DZ} + C_{EZ} + C_{NZ} = 1 \\ \end{bmatrix}$$

$$C_{[H_2O]t} = \frac{K_2 P_{AZ}^2 P_{O_2} + K_4 C_{AZ} + K_{-5} P_{H_2O} C_Z}{K_5}$$

It should be noted that the catalytic systems obtained by precipitation of the anhydrous organic ligands $C_{12}H_{10}Co-FeO_2Cl_2$ and $C_{12}H_{10}MnFeOCl_2$ on the basis of ferrosen of Co-Fe and Mn-Fe on clinoptilolite showed very high activity. At the same time rupture of the stable bond C-S in low-molecular mercaptans occurs due to process of an oxidizing reduction, and as a consequence C-S bond is cut off, resulting in formation of free sulfur and low molecular alkanes.

The mechanism of the demercaptanization process can be represented with the following equations:

A – mercaptans, z–active center of the catalyst, AZ – intermediate complex, R–CH₄H₁₀, F–C₂H₆, D – CH₂ + CH₂, E – C₂H₅OH, N – ether, M – free sulfur.

To estimate the parameters of the obtained kinetic equations can use the Arrhenius equation, i.e., depending of the rate constants and equilibrium constants of the absorption on temperature

$$K_{ef} = K_0^1 \exp(-\frac{E'_{ef}}{RT})$$
$$K_j = K_0^2 \exp(-\frac{Q}{RT})$$

Values of $E_{\rm ef}$ and $Q_{\rm i}$ – i.e. the activation energy and the absorption heat based on results of experiments were calculated on the computer in Windows XP system by method of optimization of Powell. As optimization criteria is taken the average quadratic changes of experimental and calculated data based on a kinetic model (calculated) (table 5).

$$F = \sum_{i=1}^{n} \sum_{j=1}^{m} \left[\frac{W_i^{\text{TRK}} - W_j^{\text{hes}}}{W_{ij}^{\text{TRK}}} \right]$$

 Table 5. Kinetic equation parameters of demercaptanization of ethyl mercaptan.

| K | 313 | 323 | 333 | lnK ₀ | Ε | \mathbf{Q}_i |
|-----------------------|------------------------|------------------------|------------------------|------------------|------|----------------|
| K ₁ | $0.625 \cdot 10^{-3}$ | $0.4721 \cdot 10^{-3}$ | $0.3461 \cdot 10^{-3}$ | -5.7 | - | 36.2 |
| K1 | $0.4421 \cdot 10^{-3}$ | $0.2136 \cdot 10^{-2}$ | $0.0928 \cdot 10^{-2}$ | 3.8 | - | 16.3 |
| K ₂ | $0.5432 \cdot 10^{-2}$ | $0.8341 \cdot 10^{-2}$ | $1.021 \cdot 10^{-1}$ | -4.6 | 85.6 | - |
| K ₋₂ | $0.3101 \cdot 10^{-2}$ | $0.1036 \cdot 10^{-2}$ | $0.8761 \cdot 10^{-3}$ | 6.1 | - | 20.7 |
| K ₃ | $0.7141 \cdot 10^{-3}$ | $0.9782 \cdot 10^{-3}$ | $1.3566 \cdot 10^{-2}$ | 8.2 | - | 19.4 |
| K_3 | $0.1832 \cdot 10^{-2}$ | $0.4273 \cdot 10^{-2}$ | $0.1836 \cdot 10^{-2}$ | 6.4 | - | 18.1 |
| K ₄ | $0.4321 \cdot 10^{-2}$ | $0.4321 \cdot 10^{-2}$ | $0.9861 \cdot 10^{-2}$ | -4.2 | 78.6 | - |
| K ₅ | $0.3476 \cdot 10^{-2}$ | $0.662 \cdot 10^{-2}$ | $0.8792 \cdot 10^{-2}$ | -4.0 | - | 17.2 |
| K5 | $0.1832 \cdot 10^{-2}$ | $0.6741 \cdot 10^{-2}$ | $0.0524 \cdot 10^{-2}$ | 7.4 | - | 15.4 |
| K ₆ | $0.5831 \cdot 10^{-2}$ | $0.8470 \cdot 10^{-2}$ | $1.1231 \cdot 10^{-1}$ | 5.2 | 44.2 | - |
| K ₇ | $0.6482 \cdot 10^{-2}$ | $0.9631 \cdot 10^{-2}$ | $1.3645 \cdot 10^{-1}$ | 7.1 | 74.3 | - |
| K ₈ | $0.3241 \cdot 10^{-3}$ | $0.5882 \cdot 10^{-3}$ | $0.8631 \cdot 10^{-3}$ | 5.4 | - | 18.4 |
| K8 | $0.8214 \cdot 10^{-3}$ | $0.6134 \cdot 10^{-3}$ | $0.3243 \cdot 10^{-3}$ | 3.7 | - | 16.6 |
| K9 | $0.7431 \cdot 10^{-2}$ | $0.9361 \cdot 10^{-2}$ | $1.3436 \cdot 10^{-1}$ | 5.8 | 56.2 | - |
| K ₁₀ | $0.4632 \cdot 10^{-2}$ | $0.8472 \cdot 10^{-2}$ | $1.2637 \cdot 10^{-1}$ | 4.7 | _ | 12.4 |
| K10 | $0.6334 \cdot 10^{-3}$ | $0.4641 \cdot 10^{-3}$ | $0.2144 \cdot 10^{-3}$ | 6.4 | - | 15.6 |
| K ₁₁ | $0.2112 \cdot 10^{-2}$ | $0.3641 \cdot 10^{-2}$ | $0.5634 \cdot 10^{-2}$ | -5.3 | - | 13.3 |
| K _ | $0.5542 \cdot 10^{-2}$ | $0.4133 \cdot 10^{-2}$ | $0.2234 \cdot 10^{-2}$ | 4.6 | _ | 14.8 |
| K ₁₂ | $0.4356 \cdot 10^{-2}$ | $0.7354 \cdot 10^{-2}$ | $0.9421 \cdot 10^{-2}$ | -4.4 | - | 15.8 |
| K_ 12 | $0.7648 \cdot 10^{-2}$ | $0.5331 \cdot 10^{-2}$ | $0.3754 \cdot 10^{-2}$ | 5.4 | - | 18.2 |
| - 0 | 1 • | | | • | • | - |

5. Conclusions

1.On the basis of the studied kinetic regularities data the kinetic model for the of heterogeneous catalystic process of demercaptanization of oil is developed.

2. The values of the rates of accumulation of reaction products and consumption of the initial hydrocarbon and activation energy of reactions are calculated.

3.A kinetic model is pretty well explains the experimental results and the relative error does not exceed 7-8%.

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