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# **Earth Science**

Elixir Earth Science 102 (2017) 44293-44300



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# **ARTICLE INFO**

Article history: Received: 27 September 2016; Received in revised form: 30 December 2016; Accepted: 7 January 2017;

# Keywords

Introduction

Landslides, Susceptibility, Latyan, Iran.

# ABSTRACT

The main objective of this study is to evaluate the correlated factors of landslide using certainty factor (CF) Model in Latyan catchment, north Tehran, Iran. At first, a landslide inventory map was prepared using aerial photographs and the extensive field survey. For this purpose, 208 landslides were mapped and out of which 145 (70 %) were randomly selected for building landslide susceptibility models, while the remaining 63 (30 %) were used for validating the models. In this study, 10 conditioning factors with their classes were evaluated. These factors including: slope; slope aspect; altitude; plan curvature; lithology; land use; distance from faults, rivers and roads and topographic wetness index (TWI). The validation of landslide susceptibility map was carried out using receiver operating characteristic (ROC) curve. Results shows that the slope class 20° -30 °(0.10640), slope aspect northwest (0.53335), the altitude 1800 - 2000 m (0.40805), curvature concave (0.00788), geology Jd (0.86675), Land Use forest (0.94588), distance from faults 6500–9500 m (0.47110), distance from river 0–200 m (0.25148) and distance form roads 0-500 m (0.24822) have the highest CF values. The result of ROC curve also shows that the certainty factor model has high value of AUC (0.832) which indicates the model employed in this study reasonably good accuracy in predicting the landslide susceptibility of Latyan catchment.

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Among the various land degradation process, landslides are one of the most significant phenomena. The study of landslides has drawn worldwide attention mainly due to increasing awareness of its socio-economic impact as well as the increasing pressure of urbanization on the mountain environment (Aleotti and Chowdhury 1999). The impact of artificial structures and human interventions on mountain slopes followed by expansion of agricultural land and watershed management and overgrazing has compounded the landslide disaster problem in the country. To minimize the losses of human life and economic value, potential landslideprone areas should, therefore, be identified. In this respect, landslide susceptibility assessment can provide valuable information essential for hazard mitigation through proper project planning and implementation. Landslide susceptibility is the likelihood of a landslide occurrence in an area on the basis of local terrain conditions (Brabb 1984). The advent of GIS has made the landslide susceptibility mapping easier these days (Jia et al. 2010; Karimi Nasab et al. 2010; Bednarik et al. 2012; Wang et al. 2011; Pradhan et al. 2011). Different methods to prepare landslide susceptibility and hazard mapsusing statistical methods and GIS tools were developed in the last decade (Van Westen et al. 2003; Guzzetti et al. 2005). The most common approaches proposed in the literature are bivariate (Saha et al. 2005; Pradhan et al. 2006; Magliulo et al. 2008; Pareek et al. 2010; Pradhan and Youssef 2010; Bednarik et al. 2010) and multivariate (Akgu "n et al. 2011; Pradhan 2010a; Oh et al. 2011; Choi et al. 2012). Other different methods have been proposed by several investigators, including weights-of-evidence methods (Regmi

Tele: +989174178572 E-mail address: kouhpeima@ut.ac.ir (Corresponded author) © 2017 Elixir All rights reserved et al. 2010a; Pourghasemi et al. 2012a, b), frequency ratio model (Pradhan et al. 2012), certainty factors (Pourghasemi et al. 2012a), information values (Saha et al. 2005). The aim of this paper is to produce landslide susceptibility map of Latyan catchment using certainty factor (CF) model. The model exploit information obtained from the inventory map to predict where landslides may occur in future.

### The study area

The study area is located at the north of Tehran, Iran, one of the most landslide-prone areas in Iran. The watershed area lies between the longitudes of 51° 22' to 51° 51' N and latitudes of °35 45' to °36 05' E is mountainous and lies in the geological Alborz Folded zone (fig. 1). It covers four adjacent 1:50,000 topographic sheets and has an extent of about 70793 hectares. Latyan dam is located in the study area. Climate is mountainous based on Ambrose climatically cool classification. The mean annual rainfall is around 573 mm. In general, the precipitation falls between November and January based on the records from the Iranian Meteorological Department. Altitude in the study area varies between 1,500 to 4,325m. The parts of the study area are pasture and forest and the parts utilized for orchard and agricultural and residential.

### Production of the thematic data layers

Various thematic data layers representing landslide conditioning factors namely slope, aspect, plan curvature, altitude, lithology, land use, distance from faults, distance from rivers, distance from roads, and topographic wetness index (TWI) were prepared. These factors fall under the category of preparatory factors, responsible for the occurrence of landslides in the region for which pertinent data can be collected from available resources as well as from the field.





Fig 1. Location of the Latyan catchment and landslide inventory map.

#### Landslide inventory map

The mapping of existing landslides is essential to study the relationship between the landslide distribution and the conditioning factors. In order to produce a detailed and reliable landslide inventory map, extensive field surveys and observations are performed in the study area. A total of 208 landslides are identified and mapped by evaluating aerial photos in 1:25,000 scale with well supported by field surveys (Fig. 1). The mode of failure of the landslides identified in the study area are rotational and transitional sliding according to the landslide classification proposed by Varnes (1978). Of the 208 landslides identified, randomly 145 (70 %) locations were chosen for the landslide susceptibility maps, while the remaining 63 (30 %) cases were used for the model validation. **Slope** 

The main parameter of the slope stability analysis is the slope degree (Lee and Min 2001). Because the slope degree is directly related to the landslides, it is frequently used in preparing landslide susceptibility maps (Saha et al. 2005). For this reason, the slope map of the study area is prepared from the digital elevation model (DEM) and divided into nine slope categories (Fig. 2A). An integrated land and water information system (ILWIS3.3) software was used to discover in which slope group the landslide occurred and the rate of occurrence is observed.

#### Aspect

Aspect is accepted as a main landslide conditioning factor, and this parameter is considered in several studies (Lee et al. 2004a). In this study, the aspect map of the study area is produced to show the relationship between aspect and landslides (Fig. 2B). Aspects are grouped into 9 classes such as flat, north, northeast, east, southeast, south, southwest, west, and northwest.

#### Altitude

Altitude is also a relevant landslide conditioning factor used in this study. The altitude map was prepared from the 10 m \* 10 m digital elevation model (Fig. 2C).

### **Distance from roads**

Similar to the effect of the distance from rivers, landslides may occur on the road and on the side of slopes affected by roads. Change of slope (over steepening) due to excavation, additional load, change in hydrology, and drainage may affect the stress state and slope equilibrium.

In fact, during the field works, some landslides owing to road construction work are detected. For this reason, six different buffer zones are created on the path of the road to determine the effect of the road on the stability of slope (Fig. 2D). The landslide percentage distribution and its frequency ratio are determined considering the distance classes to the road by comparing the map of the distance to the road and the landslide inventory.

### **Distance from rivers**

An important parameter that controls the stability of a slope is the saturation degree of the material on the slope. The closeness of the slope to drainage structures is another important factor in terms of stability. Streams may adversely affect stability by eroding the slopes or by saturating the lower part of material resulting in water level increases (Saha et al. 2005). For this reason, six different buffer zones were created within the study area to determine the degree to which the streams affected the slopes (Fig. 2E). Euclidean distance method was applied, and a visual inspection was done to see the correlation between the river and landslide.

#### **Distance from faults**

The distance from faults is calculated at 100-m intervals using the geological map (Fig. 2i). Euclidean distance method was applied, and a visual inspection was done to see the correlation between the faults and landslides. Faults form a line or zone of weakness characterized by heavily fractured rocks. Generally speaking, farther the distance from tectonic structures will result less numbers of landslides. Selective erosion and movement of water along fault planes promote such phenomena. A part from the major thrusts and faults derived from the geological maps, some complementary information regarding possible faults and structural dislocations was recognized as lineaments by means of image enhancement (filtering) of satellite imagery. The recognition of lineaments were performed step-by-step from large to smaller scales allowing the generalization of many neighboring small-order lineaments taking into account the spatial scale of the study (Fig. 2F).

#### Land use

Six different types of land use were described for this study using field surveys. These types of land use were pasture, forest, cultivation, Lake Dam, rocks, and residential areas (Fig. 2G). Most of the study area is covered by pasture. It is well known that land use and vegetation cover play important roles in the stability of slopes

### Plan curvature

The term curvature is theoretically defined as the rate of change of slope gradient or aspect, usually in a particular direction. The curvature value can be evaluated by calculating the reciprocal value of the radius of curvature of that particular direction (Nefeslioglu et al. 2008b). Hence, while the curvature values of broad curves are small, the tight ones have higher values. Plan curvature is described as the curvature of a contour line formed by intersecting a horizontal plane with the surface (Fig. 2H). The influence of plan curvature on the slope erosion processes is the convergence or divergence of water during downhill flow (Oh and Pradhan 2011). For this reason, this parameter constitutes one of the conditioning factors controlling landslide occurrence (Nefeslioglu et al. 2008b). The plan curvature map was produced using a system for automated geoscientific analyses (SAGA) GIS.

#### **Topographic wetness index (TWI)**

Another topographic factor within the runoff model is the topographic wetness index (TWI).

A topographic wetness index measures the degree of accumulation of water at a site (Fig. 2I).

 $TWI = \ln(a/\tan b)$ (1)

Where a is the cumulative upslope area draining through a point (per unit contour length) and tan b is the slope angle at the point. The ln(a/tan b) index reflects the tendency of water to accumulate at any point in the catchment (in terms of a) and the tendency of gravitational forces to move that water down slope (expressed in terms of tan b as an approximate hydraulic gradient). The water infiltration primarily depends upon material properties such as permeability, pore water pressure, and effects on the soil strength.

#### Lithology

The landslide phenomenon, a part of geomorphologic studies, is related to the lithology of the land. Since different lithological units have different landslide susceptibility values, they are very important in providing data for susceptibility studies. For this reason, it is essential to group the lithological properties properly (Dai et al. 2001; Duman et al. 2006). Therefore, the geological map of the study area was prepared by Geological Survey of Iran (GSI) at 1:100,000 scale and was digitized in GIS. The study area is covered with various types of lithological units. The general geological setting of the area is shown in Fig. 2J.

# Landslide susceptibility mapping

We used Certainty Factor (CF) model to obtain landslide susceptibility map. Certainty Factor (CF) is a model that has been applied by different researchers in landslide susceptibility mapping (Kanungo et al. 2011). The CF approach is one of the possible proposed favorability functions to handle the problem of combining different data layers and the heterogeneity and uncertainty of the input data. The certainty factors (CF) are given by the following equation:

$$CF = \begin{cases} \frac{ppa - pps}{ppa \times (1 - pps)} & \text{if } ppa \rangle pps \\ \frac{ppa - pps}{pps \times (1 - pps)} & \text{if } ppa \langle pps \end{cases}$$
(2)

Where CF is the certainty factor, ppa is the area of landslide events occurring in class a / the area of class a and pps is the area of all landslide events in the study area / the area of catchment. The value of the certainty factor ranges between -1 and +1. The minimum -1 means definitely false and +1 means definitely true. A positive value means an increasing certainty in landslide occurrence, while a negative value corresponds to a decreasing certainty in landslide occurrence. A value close to 0 means that the prior probability is very similar to the conditional one; hence, it is difficult to give any indication about the certainty of the landslide occurrence. The CF values for all the condition factors were calculated by overlying landslides with the parameter class, that is, by calculating the landslide density and the CF values of all the layers using Eq. 2. Next, the CF values of the landslide conditioning factors were used for creating various CF layers (Table 1). Then, the calculated CF layers were combined pairwise. The combination of two CF values, X and Y, due to two different layers of information, is expressed as Z in Eq. 3, given below:

$$z = \begin{cases} x + y - xy, & x, y \ge 0 \\ \frac{x + y}{1 - \min(|x|, |y|)}, & x, y \text{ opposite sign} \\ x + y + xy, & x, y \langle 0 \end{cases}$$
(3)

The pairwise combination is performed repeatedly until all the CF layers are added to obtain the landslide susceptibility index (LSI). To make the results easier to interpret, the LSI values are grouped into susceptibility classes to create landslide susceptibility zonation map for the study area. Several authors have applied various methods for dividing the LSI map. In this study, natural break classification method (Constantin et al. 2011; Xu et al. 2012) was used to divide the interval into five classes and a susceptibility map was prepared.

### **Results and discussion**

The CF values of all landslide conditioning factors were determined using Eq. 2. The results of spatial relationship between landslide and conditioning factors using CF model are given in Table 1. The slope class  $20^{\circ} - 30^{\circ}$  has the highest value of CF(0.10640) followed by  $65^{\circ}$  –100° class (0.04911) and 30° -65° class (0.03541) respectively. The lowest value of CF(-1) is for slope class 400–700. From this, it is clear that the landslide occurrence increases by the increase in slope percentage up to a certain extent, and then, it decreases. Few landslides occur on a very gentle slope and the landslide occurrence decreases as the slope becomes higher than  $400^{\circ}$ . In the case of slope aspect, the CF value is positive for east to northwest-facing slope facing, with the maximum value (0.53335) at northwest-facing slope followed by north-facing (0.49887) and northeast (0.22775) slopes respectively. The south-facing slopes are less prone to landslides as they have negative CF value. The CF values of altitude show that they are positive for the ranges of 1577-1800, 1800-2000, 2000-2300, and 2300-2500 with the highest value (0.40805) for the altitude ranging between 1800 and 2000 m. The CF value decreases with both the increase and decrease in altitude. It becomes negative after 2500 m. This shows that the probability of landslide occurrence decreases as the altitude becomes higher than 2500 m. In the case of curvature, the CF value is positive (0.00788) only on concave and flat slopes. The convex slopes are not responsible for landslide hazard in this area. For the geology, it can be seen that the Jd (CF =0.86675), E2ts (CF = 0.85045), Ql (CF = 0.81498), Pd (CF = 0.80082), J1 (CF = 0.79548), T1 (CF = 0.71299),  $\mathcal{E}$  bt (CF = 0.55083),Qf (CF = 0.51018), M (CF = 0.42713), Eksh (CF = 0.42178), Efsl (CF = 0.38818), Ekt (CF = 0.34381), and Qs (CF = 0.10809) are found to be more susceptible to sliding respectively (Table 1). In the case of land use, positive value of CF is seen on agricultural lands, forest lands, pasture lands and Lake Dam, while negative value of CF is seen on residential and rocks. In this case the forest lands is the highest susceptibility to landslide (CF= 0.94588) and then Lake Dam (CF=34137) is second. The high susceptibility of these two sources may be due to the human activities in the forest and the area around Lake Dam. In the case of distance from faults, the intervals 4000-6500, 6500-9500 m have weights (CF) of 0.34713 and 0.47110, respectively. Other intervals have negative CF. The influence of drainage system upon the landslide susceptibility was also analyzed by identifying the drainage river line by buffering. The distance range of 0-200 m (0.25148) has the highest CF value, followed order by 200-400 m (0.16184) and 400-650 m (0.03383).

This indicates that the landslide occurrence decreases with the increase in distance from the river. In the case of distance form roads, the intervals 0–500 (0.24822) has higher CF values, that is, the landslide susceptibility is higher in these ranges. The relation between TWI landslide probabilities showed that 12.63–24.70 class has the highest value of CF (0.17166).

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Fig 2. Thematic maps used in this study. A Slope map (%); B Aspect map; C Elevation map (m); D Distance from road map (m); E Distance from river map (m); F Distance from fault map (m); G Land use map; H Plan curvature map; I Topographic wetness index map; J Lithology map.



Fig 4. Continued

Table 1. Spatial relationship between each landslide conditioning factor and landslide by certainty factor.

| Factor               | Class          | Landslide area     | Class area | PPa     | PPs     | CF       |
|----------------------|----------------|--------------------|------------|---------|---------|----------|
| Slope degree         | 0-5            | 77.362             | 1529.478   | 0.05058 | 0.05895 | -0.14960 |
| (%)                  | 5-15           | 91.904             | 3050.289   | 0.03013 | 0.05895 | -0.50412 |
|                      | 15-20          | 21.333             | 541.817    | 0.03937 | 0.05895 | -0.34576 |
|                      | 20-30          | 68.255             | 1041.832   | 0.06551 | 0.05895 | 0.10640  |
|                      | 30-65          | 2398.300           | 39324.918  | 0.06099 | 0.05895 | 0.03541  |
|                      | 65-100         | 1481.079           | 23961.443  | 0.06181 | 0.05895 | 0.04911  |
|                      | 100-200        | 28.428             | 1157.413   | 0.02456 | 0.05895 | -0.59807 |
|                      | 200-400        | 0.144              | 3.583      | 0.04021 | 0.05895 | -0.33119 |
|                      | 400-700        | 0.000              | 0.146      | 0.000   | 0.05895 | -1       |
| Slope aspect         | Flat           | 18.676             | 631.330    | 0.02958 | 0.05895 | -0.51341 |
|                      | North          | 254.657            | 2291.711   | 0.11112 | 0.05895 | 0.49887  |
|                      | Northeast      | 709.638            | 9457.207   | 0.07504 | 0.05895 | 0.22775  |
|                      | Northwest      | 1011.998           | 8550.096   | 0.11836 | 0.05895 | 0.53335  |
|                      | South          | 411.447            | 12239.897  | 0.03362 | 0.05895 | -0.44476 |
|                      | Southeast      | 404.328            | 9497.201   | 0.04257 | 0.05895 | -0.29022 |
|                      | Southwest      | 420.847            | 12153.502  | 0.03463 | 0.05895 | -0.42744 |
|                      | East           | 493.222            | 7959.547   | 0.06197 | 0.05895 | 0.05164  |
| A 1/*/ 1             | West           | 441.985            | 7830.322   | 0.05044 | 0.05895 | -0.04515 |
| (m)                  | 1377-1800      | 403.033            | 5145.585   | 0.07833 | 0.05895 | 0.20288  |
| (m)                  | 2000 2200      | 020.300            | 12067 274  | 0.09370 | 0.03893 | 0.40000  |
|                      | 2000-2300      | 704.717<br>68/1722 | 0710 252   | 0.07393 | 0.03893 | 0.23/83  |
|                      | 2500-2500      | 436.028            | 9719.332   | 0.07045 | 0.03893 | 0.17340  |
|                      | 2700-2700      | 586 320            | 12300 1/12 | 0.04030 | 0.05805 | -0.22039 |
|                      | 2700-3000      | 164.076            | 5805 200   | 0.04732 | 0.05895 | -0.20711 |
|                      | 3200-3500      | 186 979            | 5396 221   | 0.02765 | 0.05895 | -0.42706 |
|                      | 3500-4316      | 100.902            | 3368 044   | 0.03403 | 0.05895 | -0.42700 |
| Distance from roads  | 0-500          | 1531.085           | 19904 260  | 0.02550 | 0.05895 | 0.24822  |
| (m)                  | 500-1200       | 1114 242           | 18934 538  | 0.05885 | 0.05895 | -0.00194 |
| (iii)                | 1200-2000      | 781 327            | 14666 862  | 0.05327 | 0.05895 | -0.10182 |
|                      | 2000-3000      | 509.086            | 10493 617  | 0.03327 | 0.05895 | -0.18613 |
|                      | 3000-4000      | 193.072            | 4416.998   | 0.04371 | 0.05895 | -0.27038 |
|                      | 4000-6483      | 44.547             | 2376.040   | 0.01875 | 0.05895 | -0.69502 |
| Distance from rivers | 0-200          | 1330.233           | 17223.856  | 0.07723 | 0.05895 | 0.25148  |
| (m)                  | 200-400        | 1013.387           | 14571.316  | 0.06955 | 0.05895 | 0.16184  |
|                      | 400-650        | 921.513            | 15133.258  | 0.06089 | 0.05895 | 0.03383  |
|                      | 650-1200       | 748.935            | 19812.514  | 0.03780 | 0.05895 | -0.37291 |
| Distance from faults | 0-500          | 284.316            | 6665.174   | 0.04266 | 0.05895 | -0.28876 |
| (m)                  | 500-2000       | 844.068            | 17967.967  | 0.04698 | 0.05895 | -0.21319 |
|                      | 2000-4000      | 828.255            | 20010.364  | 0.04139 | 0.05895 | -0.31077 |
|                      | 4000-6500      | 1203.165           | 13741.669  | 0.08756 | 0.05895 | 0.34713  |
|                      | 6500-9500      | 866.193            | 8178.981   | 0.10590 | 0.05895 | 0.47110  |
|                      | >9500          | 147.421            | 4228.704   | 0.03486 | 0.05895 | -0.42342 |
| Land use             | Residential    | 96.007             | 2277.587   | 0.04215 | 0.05895 | -0.29754 |
|                      | Forest         | 90.139             | 168.013    | 0.53650 | 0.05895 | 0.94588  |
|                      | Agriculture    | 410.223            | 5835.933   | 0.07029 | 0.05895 | 0.17140  |
|                      | Pasture        | 3263.313           | 53914.370  | 0.06053 | 0.05895 | 0.02762  |
|                      | Rock           | 284.797            | 8261.940   | 0.03447 | 0.05895 | -0.43012 |
|                      | Lake dam       | 29.089             | 334.909    | 0.08686 | 0.05895 | 0.34137  |
| Plan curvature       | -1.480.001     | 1469.671           | 24744.026  | 0.05939 | 0.05895 | 0.00788  |
|                      | -0.001 - 0.001 | 1136.738           | 18735.857  | 0.06067 | 0.05895 | -0.03008 |
|                      | 0.001 - 1.2    | 1566.541           | 27310.815  | 0.05736 | 0.05895 | -0.02870 |
| TWI                  | 0 - 7.67       | 1650.470           | 28601.820  | 0.05771 | 0.05895 | -0.02249 |
|                      | 7.67 - 12.63   | 1877.678           | 33107.100  | 0.05672 | 0.05895 | -0.04027 |
|                      | 12.63 - 24.7   | 638 709            | 9083 820   | 0.07031 | 0.05895 | 0.17166  |
| Lithology            | C ih           | 18.66              | 730 128    | 0.02525 | 0.05805 | -0 58655 |
|                      | Cid            | 2 12               | 172 009    | 0.02525 | 0.05075 | 0.30033  |
|                      |                | 2.13               | 1/2.008    | 0.01238 | 0.03093 | -0.79983 |
|                      | Dja            | 0.00               | 287.556    | 0       | 0.05895 | -1       |
|                      | Djv            | 0.00               | 252.628    | 0       | 0.05895 | -1       |
|                      | E 1 s          | 0.00               | 130.872    | 0       | 0.05895 | -1       |
|                      | E 1 st         | 57.41              | 1128.840   | 0.05086 | 0.05895 | -0.14471 |
|                      | E 1 tl         | 0.00               | 247.682    | 0       | 0.05895 | -1       |
|                      | E 2 ts         | 356.49             | 1207.490   | 0.29523 | 0.05895 | 0.85045  |

| E bt         | 48.15   | 393.386            | 0.12240 | 0.05895 | 0.55083  |
|--------------|---------|--------------------|---------|---------|----------|
| E bt d       | 17.00   | 579.575            | 0.02933 | 0.05895 | -0.51762 |
| Efc          | 0.00    | 239.535            | 0       | 0.05895 | -1       |
| E f sl       | 26.47   | 284.966            | 0.09289 | 0.05895 | 0.38818  |
| E f st       | 0.00    | 248.861            | 0       | 0.05895 | -1       |
| E k gt       | 0.00    | 1918.650           | 0       | 0.05895 | -1       |
| Ekm          | 102.13  | 4571.230           | 0.02234 | 0.05895 | -0.63523 |
| E k sh       | 269.50  | 2756.900           | 0.09776 | 0.05895 | 0.42178  |
| Ekt          | 1617.34 | 18557.900          | 0.08715 | 0.05895 | 0.34381  |
| E k v.t      | 0.00    | 646.552            | 0       | 0.05895 | -1       |
| E1           | 19.04   | 1162.390           | 0.01638 | 0.05895 | -0.73422 |
| Em           | 0.00    | 304.011            | 0       | 0.05895 | -1       |
| £ m2         | 0.00    | 419.260            | 0       | 0.05895 | -1       |
| E m3         | 0.00    | 556.677            | 0       | 0.05895 | -1       |
| Ev           | 0.00    | 218.665            | 0       | 0.05895 | -1       |
| £ 7          | 11.90   | 606 503            | 0.01962 | 0.05895 | -0 68053 |
| Id           | 10.67   | 33.354             | 0.31979 | 0.05895 | 0.86675  |
| Ju<br>Il     | 232 53  | 991 645            | 0.23449 | 0.05895 | 0 79548  |
| J 11         | 0.00    | 316 697            | 0.23117 | 0.05895 | -1       |
| J 12         | 0.00    | 775 642            | 0       | 0.05895 | -1       |
| K 1 12       | 0.00    | 357.048            | 0       | 0.05895 | -1       |
| K 1 12       | 0.00    | 379 318            | 0       | 0.05895 | -1       |
| K 1 V        | 0.00    | 275 579            | 0       | 0.05805 | -1       |
| M            | 77.98   | 791.021            | 0.09858 | 0.05895 | 0.42713  |
| P d          | 9.15    | 38 238             | 0.09858 | 0.05895 | 0.42713  |
| nr           | 9.15    | 58.258<br>69.744   | 0.23927 | 0.05895 | 1        |
| DE fo        | 87.40   | 3040 440           | 0 02874 | 0.05805 | -1       |
| PE fm s c    | 122.28  | 3216 220           | 0.02074 | 0.05805 | 0.32739  |
| DE v         | 0.00    | 121 642            | 0.04144 | 0.05805 | -0.30993 |
| PE 7         | 20.03   | 558 073            | 0.05104 | 0.05895 | -1       |
| Pafa         | 29.03   | 336.973            | 0.03194 | 0.05895 | -0.12346 |
| Flen         | 0.00    | 2426 700           | 0 01921 | 0.05895 | -1       |
|              | 44.01   | 2430.700           | 0.01651 | 0.05895 | -0.70231 |
| Q<br>0 1     | 86.00   | 2008 220           | 0 04227 | 0.05895 | -1       |
|              | 48.20   | 2008.330           | 0.04327 | 0.03893 | -0.27812 |
| Qai          | 40.20   | 902.943<br>549.267 | 0.03336 | 0.03893 | -0.09965 |
| QI           | 02.17   | J40.207            | 0.11340 | 0.03693 | 1        |
| Qgu          | 0.000   | 83.893<br>2170.010 | 0.06562 | 0.03893 | -1       |
| Qs           | 208.099 | 521.096            | 0.00505 | 0.05895 | -1       |
| Q sc<br>O tr | 6 101   | 183 324            | 0.03328 | 0.05895 | -0 45046 |
| Qu           | 45.851  | 1559.260           | 0.02941 | 0.05895 | -0.51641 |
| Ql           | 224.213 | 886.400            | 0.25295 | 0.05895 | 0.81498  |
| Red          | 66.300  | 1342.870           | 0.04937 | 0.05895 | -0.17099 |
| R e l        | 20.945  | 728.803            | 0.02874 | 0.05895 | -0.52769 |
| <br>R3 J s   | 133.621 | 5532.070           | 0.02415 | 0.05895 | -0.60491 |
| Тb           | 42.266  | 1019.440           | 0.04146 | 0.05895 | -0.30959 |
| T s          | 57.438  | 320.583            | 0.17917 | 0.05895 | 0.71299  |

The area of all landslides = 4174 Ha , The area of all catchment = 70793 Ha

### Validation of the landslide susceptibility maps

The landslide susceptibility map derived from model was tested using the landslide data sets that were not used in model building process. For this, the total landslides observed in the study area were split into 2 parts, 145 (70 %) was randomly selected from the total 321 landslides as the training data and the remaining 63 (30 %) landslides are kept for validation propose. Spatial effectiveness of these susceptibility maps was checked by receiver operating characteristics (ROC). The ROC curve is a useful method for representing the quality of deterministic and probabilistic detection and forecast systems (Swets 1988). The area under the ROC curve (AUC) characterizes the quality of a forecast system by describing the system's ability to predict correctly the occurrence or non-occurrence of predefined 'events'.

The model with higher AUC is considered to be the best. If the area under the ROC curve (AUC) is close to 1, the result of the test is excellent. On the other hand, if the model does not predict well, then this value will be close to 0.5. The prediction rate of the models was used for assessing the prediction capability of the models. The prediction rate explains how well the model and predictor variable predicts the landslide (Lee 2007). The prediction rate curve shows that the certainty factor model has high value of AUC (0.832) (fig.

3). From this, it is seen that the model employed in this study showed reasonably good accuracy in predicting the landslide susceptibility of the catchment.



Fig 3. Rock curve for the landslide susceptibility maps produced by CF model.

### Conclusions

Since landslides pose a serious threat to the life and property, their susceptibility mapping can be one of the preliminary steps toward minimizing the damages incurred by them. A landslide susceptibility map divides an area into various categories that range from stable to unstable ones. In this research certainty factor model was used for identifying the areas susceptible to land sliding in Latyan catchment, located in north Tehran, Iran. For this purpose, ten landslide conditioning factors (i.e., slope gradient; slope aspect; altitude; plan curvature; lithology; land use; distance from faults, rivers and roads; topographic wetness index (TWI) were used. A landslide inventory map was prepared using aerial photographs and extensive field survey. In this process, a total of 208 landslides were identified and mapped. Out of which, 145 (70 %) were randomly selected for generating a model and the remaining 63 (30 %) were used for validation proposes. The ROC plots showed that the susceptibility map produced using the model has the high perdition accuracy (83.20 %). This shows that the model employed in this study showed reasonably good accuracy in predicting the landslide susceptibility of Latyan catchment.

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